

Eqns of motion for rigid body

$$\left(\frac{d\vec{L}}{dt} \right)^F = \vec{N} \quad \text{in } F = \text{fixed IRT}$$

$$\left(\frac{d\vec{L}}{dt} \right)^F = \left(\frac{d\vec{L}}{dt} \right)^F + \vec{\omega} \times \vec{L} \quad F' = \text{(rotating) body frame}$$

$$\boxed{\left(\frac{d\vec{L}}{dt} \right)^{\text{body}} + \vec{\omega} \times \vec{L} = \vec{N}}$$

Choose body axes to be principle axes

~~moments of inertia~~

$$\vec{L} = \underline{I} \cdot \vec{\omega} \quad \vec{\omega} = \omega_i \hat{x}_i \quad L_i = I_i \omega_i \text{ etc.}$$

$$\frac{d\vec{L}}{dt} = \underline{L} \cdot \dot{\vec{x}}_i = I_i \dot{\omega}_i \hat{x}_i$$

$$\vec{\omega} \times \vec{L} = \begin{vmatrix} \hat{x}_1 & \hat{x}_2 & \hat{x}_3 \\ \omega_1 & \omega_2 & \omega_3 \\ I_1 \omega_1 & I_2 \omega_2 & I_3 \omega_3 \end{vmatrix}$$

$$\left. \begin{aligned} N_1 &= I_1 \dot{\omega}_1 - (I_2 - I_3) \omega_2 \omega_3 \\ N_2 &= I_2 \dot{\omega}_2 - (I_3 - I_1) \omega_3 \omega_1 \\ N_3 &= I_3 \dot{\omega}_3 - (I_1 - I_2) \omega_1 \omega_2 \end{aligned} \right\} \text{Euler's eqns}$$

(in rotating body frame)

$$\vec{N}_b = 0$$

Torque free motion

Start rotation about axis 1 (almost)
 $\omega_1 \gg \omega_2, \omega_3$

$$\frac{d\omega_1}{dt} = \frac{I_2 - I_3}{I_1} \omega_2 \omega_3 \approx 0 \Rightarrow \omega_1 \approx \text{const}$$

$$\begin{cases} \frac{d\omega_2}{dt} = \left(\frac{I_3 - I_1}{I_2} \right) \omega_1 \omega_3 \\ \frac{d\omega_3}{dt} = \left(\frac{I_1 - I_2}{I_3} \right) \omega_1 \omega_2 \end{cases}$$

$$\frac{d^2 \omega_2}{dt^2} \approx \frac{I_3 - I_1}{I_2} \omega_1 \frac{d\omega_3}{dt} = \left[\frac{(I_3 - I_1)(I_1 - I_2)}{I_2 I_3} \right] \omega_2$$

If I_1 is max or min moment of inertia
 $I_1 > I_3, I_2$ or $I_1 < I_3, I_2$, then

$$\frac{d^2 \omega_2}{dt^2} = -k^2 \omega_2 \quad \text{and} \quad \omega [] < 0$$

hence osc.

perturbations ~~are~~ in ω_2, ω_3 stable

If I_1 is intermediate axis, then $[] > 0$

$$\frac{d^2 \omega_1}{dt^2} = +k^2 \omega_1 \quad \text{exponential growth}$$

$\Rightarrow$ unstable

Figure for mth & figure 9 conclude

$$I_1 = I_2 = I_T$$



$$w_1 = \frac{I_T}{I_T - I_3} w_2 w_3$$

$$w_2 = - \frac{I_T}{I_T - I_3} w_1 w_3$$

$$w_3 = 0 \Rightarrow w_3 = \text{const}$$

$$w = \begin{pmatrix} I_T \\ I_T - I_3 \\ I_T - I_3 \end{pmatrix}$$

$$w_1 = \begin{pmatrix} I_T - I_3 \\ I_T - I_3 \\ I_T \end{pmatrix} w_2 w_3$$

$$w_1 = A \cos(\Omega t)$$

$$w_1 = -A \Omega \sin(\Omega t) = -\Omega w_2$$

$$\Rightarrow w_2 = +A \sin(\Omega t)$$

$$w_T = \sqrt{w_1^2 + w_2^2} = A, \text{ const}$$

$$\Omega = \begin{pmatrix} I_3 - I_1 \\ I_3 - I_1 \\ I_T \end{pmatrix} w_3$$

$$\frac{I_T}{I_3 - I_1} \approx \frac{1}{300}$$

$$I_3 \approx I_1 \text{ Earth}$$

~~570~~ for part K

Precession about X_3

ω / $\text{freq } \Omega$

$$\text{For } K: \Omega = \frac{300}{\omega_3}$$

$\Rightarrow \text{period} = 300 \text{ days}$

(Chandler wobble
~ 400 days)

$$\omega = \omega \cos \alpha$$

$$\omega_T = \omega \sin \alpha$$

$$L_3 = I_3 \omega_3 = I_3 \omega \cos \alpha$$

$$L_T = I_T \omega_T = I_T \omega \sin \alpha$$

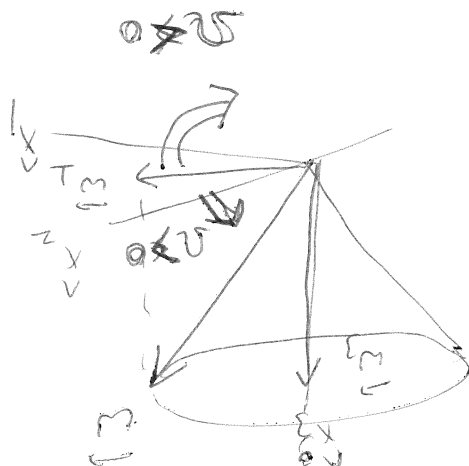
$$\frac{L_T}{L_3} = \frac{I_T}{I_3} \tan \alpha$$

$$I_3 > I_1 \Rightarrow \theta < \alpha \text{ (small)}$$

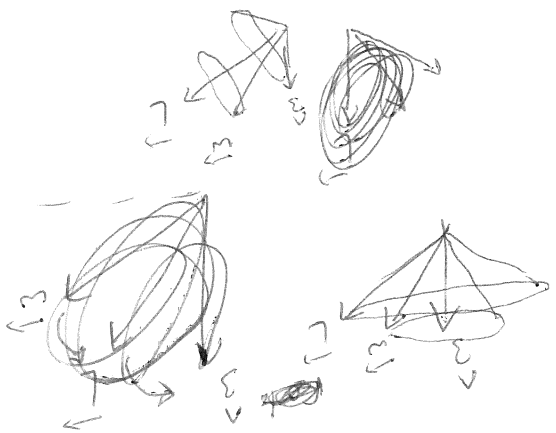
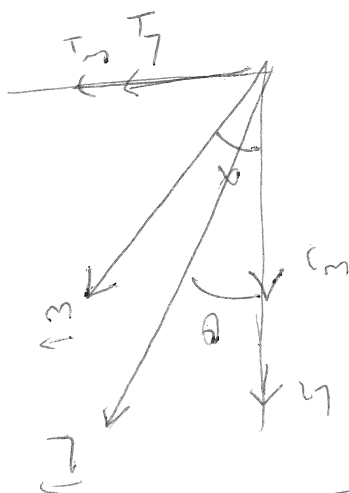
$$I_3 < I_1 \Rightarrow \theta > \alpha$$

In rotating frame $\vec{\omega} \perp \vec{L}$ precesses about X_3 w/ $\text{freq } \Omega$

In fixed frame $\vec{L} = \text{const}$ and $\vec{\omega}$ and X_3 precess about it



Angular momentum



$$\text{max. } \pi = 0.5 \phi^T I = 0.50 \text{ t} - \phi \phi$$

$\frac{d\phi}{dt} = \frac{e}{T_e} = \phi \frac{d\phi}{dt}$

$$\left. \begin{aligned} \omega_3 &= \psi + \phi \cos \theta \\ \omega_1 &= \phi \cos \psi + \phi \sin \theta \sin \psi \\ \omega_2 &= \phi \sin \theta \cos \psi - \phi \sin \psi \end{aligned} \right\} \rightarrow \text{in this argument}$$

$$\frac{3}{2} m \frac{3}{2} I \frac{2}{T} + \left(\frac{2}{2} m + \frac{1}{2} m \right) T I \frac{2}{T} = T$$

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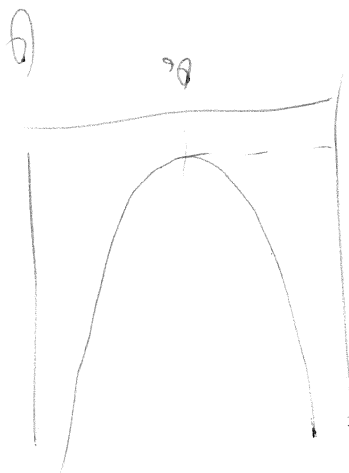
$$\left(\frac{p_4^2}{4mgh I \cos \theta_0} - 1 \right) \mp 1 \left(\frac{2 \cos \theta_0}{p_4 \sin \theta_0} \right) = \beta$$

$$\beta = p_4 - p_4 \cos \theta_0$$

$$0 = \beta (p_4 \sin \theta_0) - \beta^2 (\cos \theta_0) - I mgh \sin \theta_0$$

Consider $\theta = \theta_0 = \text{const}$

$$\frac{\partial V_{\text{eff}}}{\partial \theta} = 0 = \frac{\partial}{\partial \theta} \left[\frac{I \sin^2 \theta}{(p_4 - p_4 \cos \theta)^2} (p_4 \sin \theta) - \frac{I \sin^2 \theta}{(p_4 - p_4 \cos \theta)^2} \cos \theta - mgh \sin \theta \right]$$



$V_{\text{eff}}(\theta)$

$$= \frac{1}{2} I \dot{\theta}^2 + \left[\frac{2 I \sin^2 \theta}{(p_4 - p_4 \cos \theta)^2} + mgh \cos \theta \right]$$

$$= \frac{1}{2} I \dot{\theta}^2 \left(\left[\frac{I \sin^2 \theta}{(p_4 - p_4 \cos \theta)^2} \right] \sin^2 \theta + \theta^2 + \theta^2 \sin^2 \theta + \frac{1}{2} \frac{I}{p_4^2} + mgh \cos \theta \right)$$

$$\left(\frac{I}{p_4^2} \right)^2$$

$$E = \frac{1}{2} I \dot{\theta}^2 \left(\phi^2 \sin^2 \theta + \theta^2 + \theta^2 \sin^2 \theta + \frac{1}{2} \frac{I}{p_4^2} + mgh \cos \theta \right)$$

~~Equation~~

$$\Rightarrow \phi = \frac{I_{\text{enc}}}{\epsilon_0} = \frac{I_{\text{enc}}}{\epsilon_0} \quad \text{plan pac}$$

$$= \frac{I_{\text{avg}}}{P_T} = \phi \quad (=)$$

$\frac{p_2}{p_1} = \frac{v_1}{v_2}$

long + d $\Leftarrow$ long con = def friends very reding

you need $\geq$ 4 wgs $\Rightarrow$

Let θ parameter: $\phi = \beta^T I \sin \theta$

$$I_{mJ} = \phi$$

$$\omega_3 \geq \frac{I_3}{2} \sqrt{mgh I_3 \cos \theta_0}$$

Minimum Spots
to be covered

$$I_{3m} \geq I_{2m} = I_{3m}$$

$$\beta_{\text{mod}} \leq 1 - \frac{p_2}{4mgk \pm \text{const.}}$$