

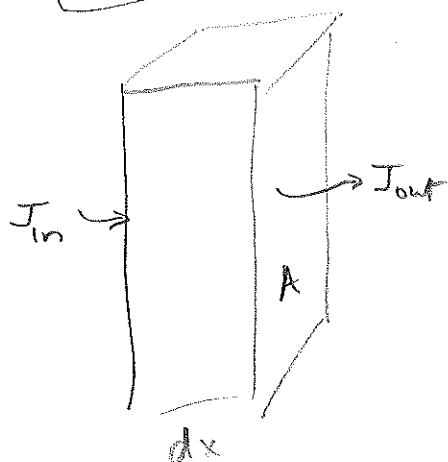
Thermal diffusion (one dimension)

Recall heat current density $J_h = \frac{\text{(energy)}}{\text{(area)}(\text{time})}$

Flow of thermal energy is driven by temperature difference

$$(1) \quad J_h = -k \frac{\partial T}{\partial x}$$

(Fourier's law) $k = \text{thermal conductivity}$



If $J_{in} > J_{out}$, energy builds up in slab

Define thermal energy density $\rho_h = \frac{\text{(energy)}}{\text{(volume)}}$

Thermal energy in slab $= \rho_h A dx$

change in energy per time = net inflow of energy

$$\begin{aligned} \frac{\partial \rho_h}{\partial t} A dx &= (J_{in} - J_{out}) A \\ &= [J_h(x) - \underbrace{J_h(x+dx)}_{J_h(x) + \frac{\partial J_h}{\partial x} dx}] A = -\frac{\partial J_h}{\partial x} dx A \end{aligned}$$

$$(2) \quad \boxed{\frac{\partial \rho_h}{\partial t} = -\frac{\partial J_h}{\partial x}} \quad \text{"continuity equation" (energy conservation)}$$

Combine (1) + (2) $\Rightarrow$ (3) $\boxed{\frac{\partial \rho_h}{\partial t} = k \frac{\partial^2 T}{\partial x^2}}$

change in thermal energy is proportional to change in temperature

$$\Delta p_h A dx = C \Delta T$$

C = heat capacity of slab

define specific heat c = heat capacity per unit mass

Then $C = c \cdot \rho_m \cdot A dx$, where ρ_m = mass density

$\downarrow \quad \quad \downarrow \quad \quad \downarrow$
 $\left(\frac{\text{heat capacity}}{\text{mass}}\right) \left(\frac{\text{mass}}{\text{vol.}}\right) (\text{volume of slab})$

$$\Rightarrow \Delta p_h = c \rho_m \Delta T$$

$$(4) \quad \boxed{\frac{\partial p_h}{\partial t} = c \rho_m \frac{\partial T}{\partial t}}$$

Combine (3) + (4)

$$c \rho_m \frac{\partial T}{\partial t} = k \frac{\partial^2 T}{\partial x^2}$$

$$\boxed{\frac{\partial T}{\partial t} = D \frac{\partial^2 T}{\partial x^2}}$$

one dim'l heat diffusion eqn

where D = thermal diffusivity = $\frac{k}{c \rho_m}$

Not for class

$\left. \begin{array}{l} \text{Cu} \\ k = 0.93 \frac{\text{cal}}{\text{cm} \cdot \text{s} \cdot ^\circ\text{C}} \\ C = 0.0923 \frac{\text{cal}}{\text{g} \cdot ^\circ\text{C}} \\ \rho = 8.960 \text{ g/cm}^3 \end{array} \right\} D = 1.12 \text{E-}4 \frac{\text{m}^2}{\text{s}}$

$\left. \begin{array}{l} \text{H}_2\text{O} \\ k = 0.58 \text{ J/m} \cdot \text{s} \cdot ^\circ\text{C} \\ C = 4.185 \text{ J/g} \cdot ^\circ\text{C} \\ \rho = 10^6 \text{ g/m}^3 \end{array} \right\} D = 1.4 \text{E-}4 \frac{\text{m}^2}{\text{s}}$

Steady-state distribution in 1 dimension

means T depends on x , not t

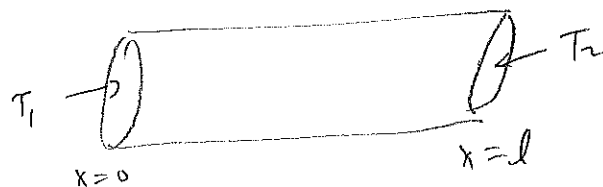
$$\frac{\partial T}{\partial t} = 0 \Rightarrow T = T(x)$$

$$\text{Then diffusion equation} \Rightarrow \frac{d^2 T}{dx^2} = 0$$

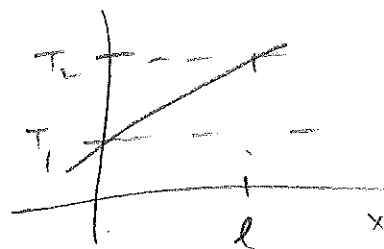
$$\frac{dT}{dx} = A$$

$$T = Ax + B$$

Use boundary conditions to determine A & B



$$T(x) = T_1 + (T_2 - T_1) \frac{x}{l}$$



Non steady state heat flow

2-D4

$$\frac{\partial T}{\partial t} = D \frac{\partial^2 T}{\partial x^2}$$

[2nd order linear PDE (2 indep vls x, t)]

Try separable ansatz $T(x, t) = f(x) g(t)$

Strategy: ① substitute ansatz into PDE
② divide by ansatz + simplify
③ observe that each term is separately constant

$$① \quad f g = D g f''$$

$$\dot{g} = \frac{dg}{dt}$$
$$f'' = \frac{d^2 f}{dx^2}$$

$$② \quad \frac{\dot{g}}{g} = \frac{D f''}{f}$$

$$③ \quad \frac{f''}{f} = \frac{1}{D} \frac{\dot{g}}{g}$$

only depends on x indep of x $\therefore \frac{f''}{f} = \text{const}$

Is the constant positive or negative? B.c. - will force it to be negative.

$$\text{Let } \frac{f''}{f} = -k^2$$

$$\frac{\dot{g}}{g} = -k^2 D$$

$$\frac{d^2 f}{dx^2} + k^2 f = 0$$

$$\frac{dg}{dt} + k^2 D g = 0$$

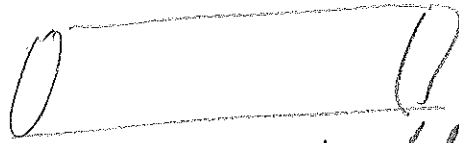
$$f = A \cos kx + B \sin kx$$

$$g = e^{-D k^2 t}$$

$$\Rightarrow T(x, t) = (A \cos kx + B \sin kx) e^{-D k^2 t} \quad \text{solve PDE}$$

Apply boundary conditions

2.55



Suppose both ends held at $T=0$ for $t \geq 0$

$$T(0, t) = A e^{-Dk^2 t} = 0 \Rightarrow A = 0$$

$$T(l, t) = B \sin(kl) e^{-Dk^2 t} = 0 \Rightarrow B = 0 \text{ or } kl = n\pi$$

$$k_n = \frac{n\pi}{l}$$

General solution

$$T(x, t) = \sum_{n=1}^{\infty} B_n \sin(k_n x) e^{-Dk_n^2 t}$$

Apply initial conditions:

Suppose rod has initial temperature distribution $T_0(x)$

$$T(x, 0) = \sum B_n \sin(k_n x) = T_0(x)$$

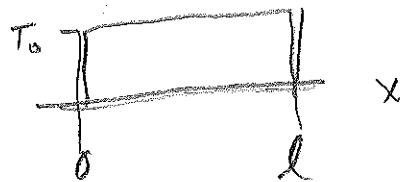
↑
Fourier coefficients

$$B_n = \frac{2}{l} \int_0^l T_0(x) \sin(k_n x) dx$$

Suppose rod is heated to a uniform initial temp T_0

then at $t \geq 0$, both ends are held at $T=0$.

Assume sides are thermally insulated so
no heat flows laterally



$$B_n = \frac{2}{l} T_0 \int_0^l \sin\left(\frac{n\pi x}{l}\right) dx$$

$$= \frac{2}{l} T_0 \left[-\frac{l}{n\pi} \cos\left(\frac{n\pi x}{l}\right) \right]_0^l$$

$$= \frac{2T_0}{n\pi} [1 - \cos(n\pi)]$$

$$= \frac{4T_0}{\pi n} \sin^2\left(\frac{n\pi}{2}\right) = \begin{cases} \frac{4T_0}{\pi n}, & n \text{ odd} \\ 0, & n \text{ even} \end{cases}$$

$$T_0(x) = \frac{4T_0}{\pi} \sum_{n \text{ odd}} \frac{1}{n} \sin\left(\frac{n\pi x}{l}\right)$$

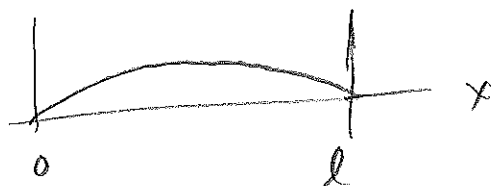
$$= \frac{4T_0}{\pi} \left[\sin\left(\frac{\pi x}{l}\right) + \frac{1}{3} \sin\left(\frac{3\pi x}{l}\right) + \dots \right]$$

see composite square on Blackboard

$$T(x,t) = \frac{4T_0}{\pi} \sum_{n \text{ odd}} \frac{1}{n} \sin\left(\frac{n\pi x}{l}\right) e^{-n^2 \left(\frac{\pi^2 D}{l^2}\right) t}$$

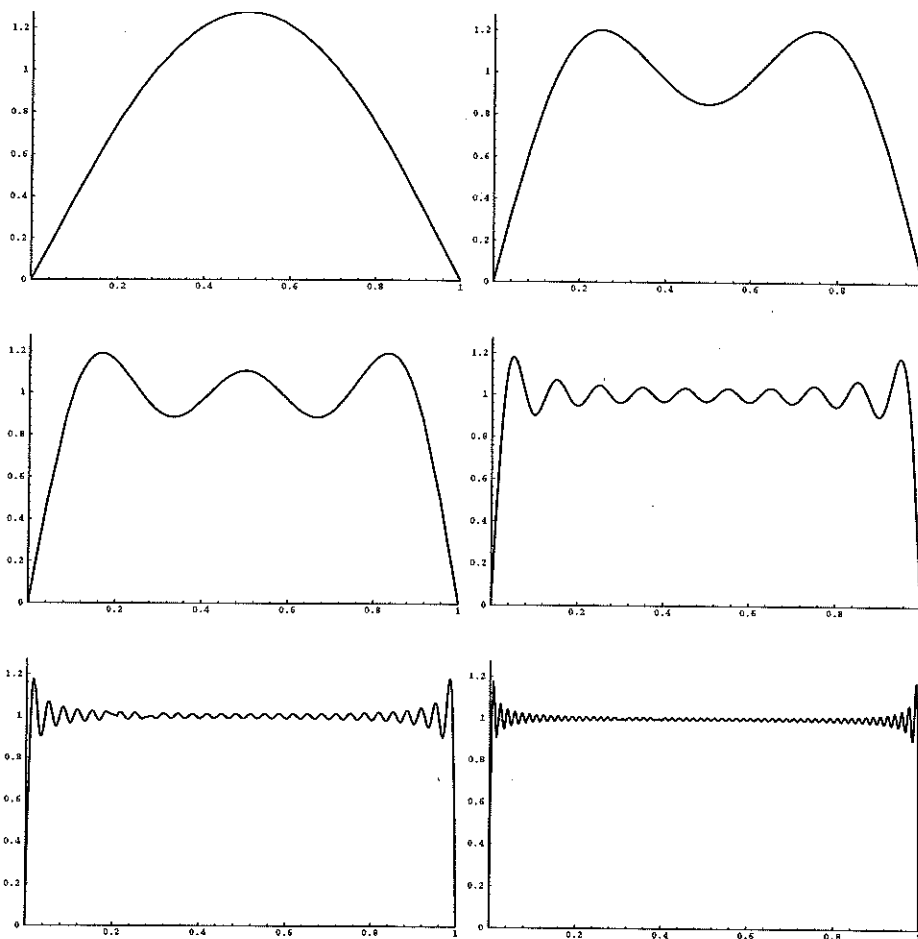
$$= \frac{4T_0}{\pi} \left[\sin\left(\frac{\pi x}{l}\right) e^{-\frac{\pi^2 D t}{l^2}} + \frac{1}{3} \sin\left(\frac{3\pi x}{l}\right) e^{-\frac{9\pi^2 D t}{l^2}} + \dots \right]$$

higher terms die off quickly



see relaxation on Blackboard

```
partial[m_,t_]=4/Pi*Sum[Sin[(2n+1) Pi x]*Exp[-(2n+1)^2 Pi^2 t]/(2n+1), {n,0,m}]
Display["!psfix > sq60.eps", Plot[partial[59,0],{x,0,1},
PlotRange->{{0,1}, {0,4/Pi}}]]
```



clamped-square

*← 18%
over shoot*

Figure 1: Fourier decomposition of square wave with 1, 2, 3, 10, 30, and 60 terms

relaxation.nb

```
in[7]:= amp = 4 / Pi;
```

```
in[8]:= mode[x_, t_, n_] = amp / n * Sin[n * Pi x] * Exp[- (Pi n)^2 t];
```

```
in[9]:= partialsum[x_, t_, m_] := Sum[mode[x, t, n], {n, 1, m, 2}];
```

```
in[10]:= Animate[  
  Plot[partialsum[x, t, 119], {x, 0, 1}, PlotRange -> {{0, 1}, {0, 1.2}}, {t, 0, .5}]
```

↳ 60 terms

OBSCURE TO

from
composite-square-wave
[after Vand (document)]

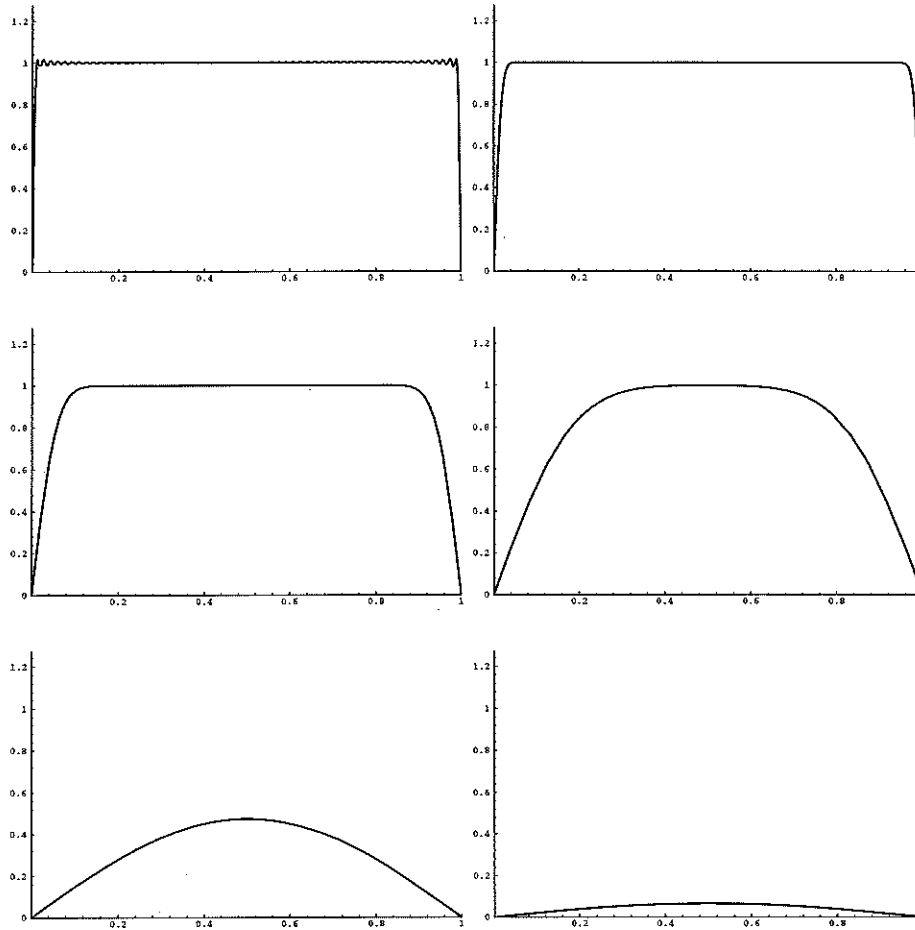
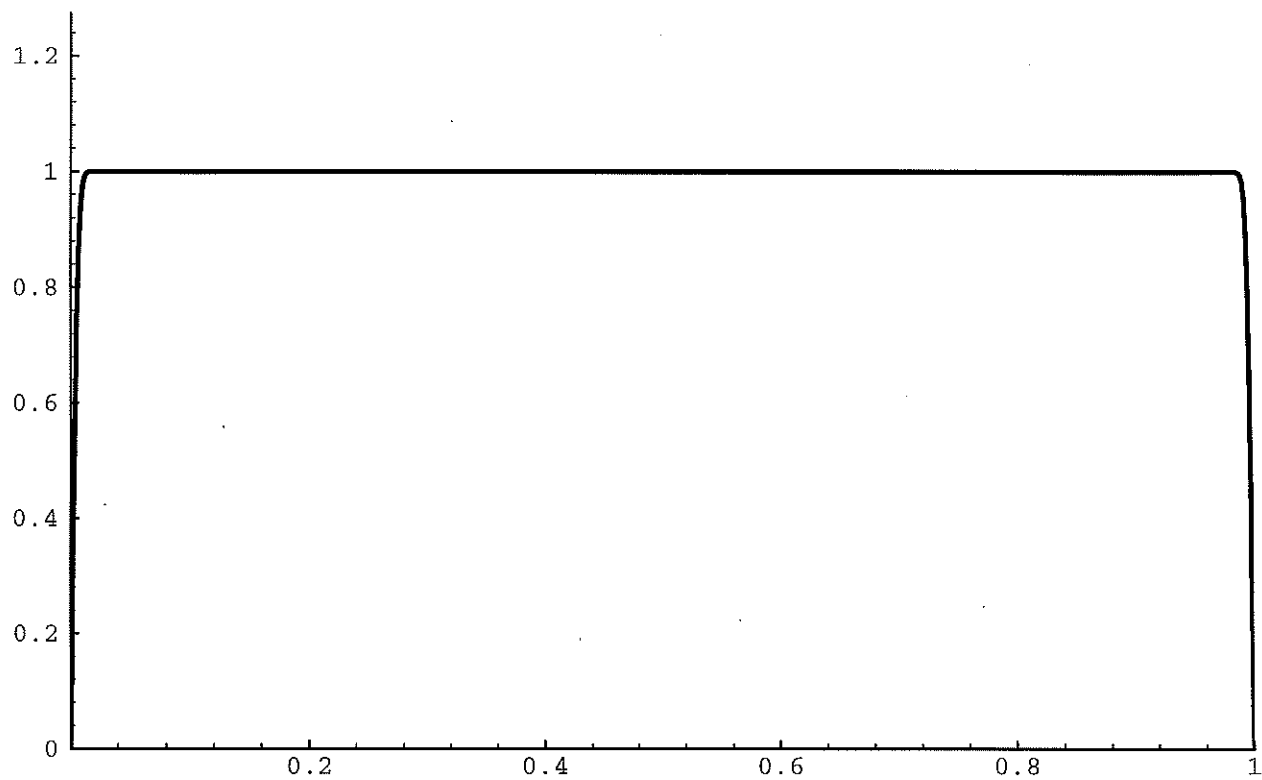


Figure 2: Thermal time evolution of square wave (with 60 terms) at $t = 10^{-5}$, 10^{-4} , 10^{-3} , 10^{-2} , 10^{-1} , and 0.3

$t = 0.00001$
w/ 160 terms in
Fourier series



Other possible topics

✓ Now a problem

If one end of rod held at $T=0$ and other at $T=T_0$
find $T(x,t)$ given initial profile

Since steady-state soln is $T_0 \frac{x}{l}$
subtract this from initial profile & solve

[discussed in 5'02]

Insulated ends: $\frac{\partial T}{\partial x} = 0$ at $x=0$

↗ use cos()

Neumann b.c.